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Copyright 2003, 2005 by John Wiley & Sons 1 Solutions to Supplementary trouble keeping up with the 3rd Edition of Power Electronics: Converters, Applications and Design by Ned Mohan, Tore Undeland, and William Robbins Copyright 2002 Copyright 2003, 2005 by John Wiley & Sons 2 chapter 1 - Power Electronic Systems S1.1. In linear Electronics Sa f semiconductor devices used in the middle of its regiÅpes of the linear amplificaÅÅ f, where both the voltage E © s atravÁ component and current atravÁ it sÁ f © s relatively large. This results in high power dissipation of the f. In potÁªncia of Electronics, f semiconductor devices are used as the switches. When the device is in (a f the aproximaÅÅ a closed switch) to the voltage atravÁ E © s device to very low (typically 1-3 volts mÁximo) and the current atravÁ s © s it the large. The dissipation f the potÁªncia, substantially at the same time, © much less than the operating regia E f amplificaÅÅ the linear at the same current navel. When the device © off (aproximaÅÅ one o f an open switch) to the voltage atravÁ E © s component A are large, but the current is very small and © E dissipation in the off state potÁªncia It can usually be considered as zero. S1.2. 1. advancements in microelectrªnica that allow the fabrication f high-performance controllers in both digital and both analog forms. 2. Improvements in the capabilities revolutionary (f the voltage, current, power dissipation and the f speeds comutaÅÅ E o) of semiconductor devices that function as switches in power converters electrªnicos. 3. Great expansa E eletrªnicos the converters market potÁªncia. S1.3. The table below features the Åreas of aplicaÅÅ E o, in terms of matters concerning INSTANCE ¢ or priority Electronics designer potÁªncia should put in each of the listed specs. The assessments in the table sÁ f highly qualitative. E AplicaÅÅ the Pwr Evaluation f Dynamics Cost Efficiency Size and Weight Residential Copyright 2003, 2005 by John Wiley & Sons 3 S1.4. a) Figure 1-3a already estÁj diagrammed showing that the converter has two rectifiers, an inverter, a transformer and two energy storage capacitors. b) Block Diagram shown below. Rectifier & filter inverter Rectifier low pass & low pass filter Utility Controller Load Vref Vo Safety Isolation Copyright 2003, 2005 by John Wiley & Sons 4 chapter 2 - f Vision general of semiconductor switches S2.1 potÁªncia. a) Ideal i-v curves for a diode and a thyristor sÁ f shown below. A more complete Number for dÁodo Å © shown in Fig. 2-1 text and the thyristor, Fig. 2-3 text. b) Characteristics sÁ f ideal when used bÅjsico the operation of a converter circuit estÁj to be analyzed or designed from a viewpoint from above (system). This situaÅÅ E o, the idealized characteristics greatly simplify the esforÅo ManiMa with loss of precision E o. The characteristics nÁ E f the ideal What sane disposed in the sÁ f idealizaÅÅÅpes the second order effects which tÁªm-Only minor effects on the general characteristics of the converter. The actual characteristics used sÁ f Å when the actual effects of the estimated f sÁ characteristics. These effects sÁ f usually the most important in prÁªprio device and may cause the device to mÁiximas capacity being exceeded. For example, the Resistance in the state of a dÁodo a caracterÁstica nÁ E o-optimal, causes the dissipation f potÁªncia the diode when it estÁj in the state. An accurate knowledge of the energy losses Å © Required to properly scale the heat sink. If the dissipation f potÁªncia exceed the potÁªncia mÁxima dÁodo, the diode may exceed the internal temperature mÁximo admissÁvel value and at least the reliability of dÁodo serÁj significantly reduced. S2.2. a) E the diode voltage and the voltage endurance E load shown below. iv Ideal diode curve iv iv curve 0 Ideal thyristor V322 V322 Vinput Voltage 322 V0 VLoad VOLTAGE 20 MILLSECONDS DIOD VOLTAGE-322 V0 VTTCOPYRIGHT 2003, 2005 by John Wiley & Sons 5 Vd = 10,02 00.01326sin (2x50t) DT = 322 = 102 volts b) Devices in parallel have the same impressed voltage through them. The device with the inferior tension is through it for a given current, will will a chain larger than other paralleled devices. This means that the current transport device will dissipate more energy than other paralleled devices. Consequently, the temperature will be higher in this device than on other devices. This higher temperature will lead to an even greater portion of the current through this device. The end result may be that the current in this device may exceed the classification of the device. Copyright 2003, 2005 by John Wiley & Sons 6 Chapter 3 - Revision of Basic Concepts S3.1. a) The input voltage shown below. 30 v6 s4 s 2 st0v1 in the state station, there is no meaning of the inductor in the way the man of v1 is equal to the mother of vo. = (30) (4) 6 = 20 V = VO. b) 250 w = (20) 2R, r = 400250 = 1.6; (fo) 2 (1.6) = 250; IO = 2501.6 = 12.5A C) Tension Inductor = VI (T) - You are assumed that the variable portion with the time of the skirt voltage is very small (C very large). Hence inducing tension and chain waveforms are shown below. For the VL (t) = Idl (t) dt inducer. During the time intervals when the tension is constant inducer, the inductor will change linearly over time. During the 4 s interval the current in the inductor = i1 + 10 v 5 h t = i1 + 2x106 t at the end of the 4 sec interval i1 + 8 = i2 or i2 - i1 = 8 a mother current = IO = 12.5 = I1 (6s) + (8a) (4S) (0.5) + (8-a) (2S) (0.5) 6 S = i1 + 4a So i1 = 8.5AE I2 = 16.5 A Copyright 2003, 2005 by John Wiley & Sons 7 10 V6 S4 S Two R-20 VVITI1121 (t) = 12.5 LIU A = +

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